On-line Computation of a Local Attainable Moment Set for Reusable Launch Vehicles*

A. S. Hodel[†]

Yuri B. Shtessel[‡]

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Extended Abstract

Problem description Traditional attitude control design of reusable launch vehicles involves independent design of autopilot and control allocation modules [SBB99], [SK97], [SHJ00], [PS00], [Hod00]. Unfortunately, this results in the potential for overly aggressive commands in the autopilot resulting in a loss of performance due to actuator saturation, particularly if the autopilot may suffer from integrator wind-up [HH01]. This unfortunate situation can arise from, e.g., actuator position limits that require that the actuator command vector $\delta_c(t) \in \Delta$ where Δ is the set of feasible actuator commands defined by

 $\Delta \stackrel{\Delta}{=} \{\delta : \delta_{-} \leq \delta \leq \delta_{+}\}$

where δ_{-} and δ_{+} are minimum and maximum position commands, respectively. Control allocation is limited by the attainable moment set \mathcal{T} [BD95], [Dur93], [Dur99], defined as

$$\mathcal{T} = \{\tau: \exists \delta \in \Delta \text{ and } G\delta = \tau\}$$

where G is the current Jacobian (control derivatives) matrix from the vehicle actuator condition vector
t δ to the vehicle body torques τ_b

 $G \triangleq \frac{\partial \tau_b}{\partial \delta}$

On-line calculation of the entire attainable moment set $\mathcal T$ is not a practical option for the following reasons:

- 1. Actuator models (aerodynamic) are approximate at best.
- 2. Actuator failure will significantly modify the attainable moment set \mathcal{T} .

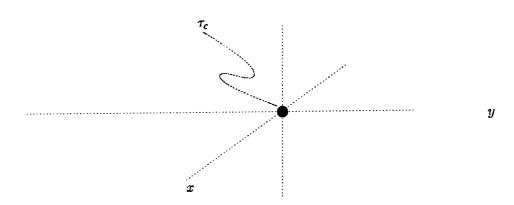
We propose instead to calculate a point-wise "snapshot" of $\mathcal T$ as shown in Figure 1. Given a torque command τ_c we compute a local attainable moment set $\mathcal{T}(\tau_c)$ determining the maximum and minimum torque limits in each channel (x = roll, y = pitch, z = yaw) while holding the other torque

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[†]a.s.hodel@eng.auburn.edu, Dept. Elect. & Comp. Eng., 200 Broun Hall, Auburn University, Auburn, AL 36849-5201, corresponding author.

[‡]Department of Electrical and Computer Engineering, University of Alabama at Huntsville.

Normal vector to surface



z

normal vector to surface

Figure 1: Attainable moment set snapshot

values constant. The dimensions of this local attainable moment set can be calculated by a linear programming problem, e.g., given the current system Jacobian matrix G,

$$\begin{array}{rcl} \tau_{x,\max} &=& \arg\max_{\delta} \left[\begin{array}{ccc} 1 & 0 & 0 \end{array} \right] G \delta \\ \\ & \text{subject to} \ \ \delta \in \Delta, \ \left[\begin{array}{ccc} 0 & 1 & 0 \\ 0 & 0 & 1 \end{array} \right] G \delta = \left[\begin{array}{ccc} 0 & 1 & 0 \\ 0 & 0 & 1 \end{array} \right] \tau_{c} \end{array}$$

These torque limits may be of use in two scenarios:

- 1. in communicating overall actuator torque limits to the autopilot and autocommander so that autopilot and/or guidance commands may be appropriately adjusted, and
- 2. in flight scenarios where control allocation is required to divide torque commands a primary set of actuators (e.g., aerosurfaces) and a secondary backup set of actuators (e.g., reaction thrusters).

Torque limits computation and linear programming The computation of the local attainable moment set can be posed as a set of six linear programming problems

$$\max_{x} J(x) \qquad J(x) = c^{T} x$$
subject to
$$Ax = b$$

$$x^{-} \le x \le x^{+}$$

$$(0.1)$$

where c^T and A are construct from appropriate rows of the Jacobian matrix G and the vector b is the set of "pinned" torques from the current (feasible) torque command τ_c . (If τ_c is infeasible then torque limits max J(x) can be computed by locating the vertex of the feasible set that minimizes the error Ax = b [Luc84].) Standard codes ¹ available for the linear programming problem such as dsplp and lp_solve are inappropriate for this problem, since

- 1. These codes are design for large sparse problems, where as our A matrix is dense and we have very few unknowns - at most 10 or 20.
- 2. These algorithms can require several iterations to converge to an optimal solution, where as we require fast operation (low computational overhead).
- 3. Our problem does not change too much from one time-step to the next (system Jacobians do not change much over one sampling period), so our method should make use of earlier solutions.
- 4. Further, our problem does not require an exact optimal solution just a good approximation.

We therefore propose the use of a limited-iteration simplex method LP solution that uses results (active constraint set) of the previous iteration to compute initial values for the next iteration. Experience indicates that two simplex iterations is sufficient for adequate performance, and so our method requires the inversion of at most 24 2 × 2 matrices (2 for each limit, 2 limits per axis).

We show preliminary results of our method in Figure 2. The routine lpsolve is a full simplex LP solver that exits upon convergence or detection of an infeasible problem (notice time spike at $t \approx 13 \mathrm{sec}$). The routine lpIter is an implementation of our fast LP solver. Both lpsolve and lpIter have an outermost m-file script that is used to call a C-code implementation of our fast iteration. dmTrqLim is a full C-code translation of lpIter that is included for comparison. Observe that, except when the input torque command is infeasible, lpIter closely tracks that achievable torque limits even though it is limited to at most two simplex iterations per time step. This example was run with only 6 simulated actuators; similar results were obtained with much larger numbers of actuators in other simulation tests.

These torque limits can then be used to adjust autopilot control parameters on-line so that the autopilot can respond appropriately to either saturations or permanent failures. One potential method for using torque limits is presented explicitly in [SBB99]. We are investigating the use of this method in closed-loop control simulations of the X-33 launch vehicle.

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search on www.netlib.org or on google for keywords "linear programming")

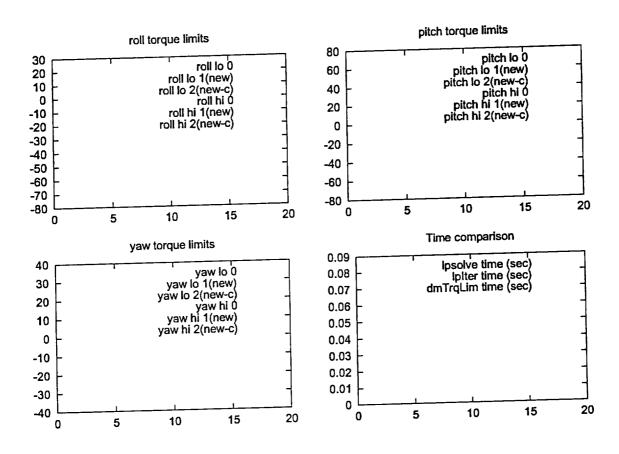


Figure 2: Preliminary test results for fast computation of the local attainable moment set. Plant Jacobians were made to vary sinusoidally. An artificial failure (zero effectiveness) was simulated at $t=10{\rm sec}$. Simulation experiments were performed with C-code integrated into Octave on a 450 MHz Macintosh running Yellow Dog Linux v 2.0.

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